

About this Article

This material was included with the downloadable supplemental content accompanying the *ARRL Antenna Book*.

You may print a copy of this material for personal use. Any other use of the information requires permission from the ARRL.

Copyright/Reprint Notice

In general, all ARRL content is copyrighted. ARRL articles, pages, or documents – printed and online – are not in the public domain. Therefore, they may not be freely distributed or copied. Additionally, no part of this document may be copied, sold to third parties, or otherwise commercially exploited without the explicit prior written consent of the ARRL. You cannot post this document to a website or otherwise distribute it to other through any electronic medium.

For permission to quote or reprint material from ARRL, send a request including the issue date, a description of the material requested, and a description of where you intend to use the reprinted material to the ARRL Editorial and Production staff at: **permission@arrl.org**.

The AMRAD Active LF Antenna

You can tune into LF activity with this easy-to-build and erect active antenna. As a bonus, you get MF and HF coverage, too—not to mention world-class performance!



The Amateur Radio Research and Development Corporation (AMRAD) is a nonprofit radio club that specializes in cutting-edge—yet fun—Amateur Radio technology. In a jump back to the future, several of us decided to look into low-frequency radio (LF). Many European countries now have an Amateur Radio allocation at 136 kHz, and AMRAD, hoping for a future FCC amateur allocation there—obtained an FCC Part 5 license to operate experimentally on those challenging low frequencies. Many hams wanted to listen to our transmissions, but lacked a suitable receiving antenna. The antenna described here should do nicely.

Some Background

The evolution of our present antenna has a proud lineage. AMRAD member Dick (WA3USG) Goodman's Monster Loop is an excellent antenna and met our initial need.¹ Another member, Bill Farmer, W3CSW, built a loop antenna in his attic that also performs well.² Low-frequency veteran Ken Cornell, W2IMB, described several active antennas, including his varactor-tuned active antenna.³ And engineering whiz Andre Kesteloot, N4ICK, presented an even better design. His varactor-tuned active antenna has the tuning stage *ahead* of the FET follower.⁴ N4ICK's antenna works very well, but like the Cornell design, it must be tuned to the desired frequency. Because of their simplicity and performance, Ralph Burhans' active-antenna designs became popular

with LOWFers (low-frequency experimenters) in the 1980s.^{5,6} Even though they're a few years old, Burhans' articles provide important information about the workings of active antennas. These antennas were a starting point in our quest for an improved LF active antenna.

The US Navy gave the club access to some large LF *transmitting* antennas that were scheduled for demolition. We conducted a series of tests and concluded that for LF receiving, a well-designed active antenna in a low-noise area can perform as well as much larger antennas.⁷

This Project

The active antenna described here can be a powerful tool for the future LF-active ham seeking to work Europe and win the *Bobek LF Transatlantic Challenge* (once an LF Amateur Radio band is allocated by the FCC, of course). For more information about the Challenge, see

www.g3wkl.freemove.co.uk/awards/136_trans_challenge.html.

We set out to build a transatlantic-grade LF antenna that any ham could build with simple hand tools. We also wanted our design to improve on Burhans' IMD performance to enable urban hams to receive the LF bands without dealing with spurious signals caused by IMD. We also wanted our antenna to work to 30 MHz, if possible, to make the antenna generally more useful. We're pleased to report that this antenna exhibits improved IMD performance and has a useful range of 10 kHz to 30 MHz.

What is an Active Antenna?

An active antenna is an electrically and physically small antenna combined with an active electronic circuit, such as an amplifier. An active antenna, like the one described here, uses a small whip—one that is a fraction of a wavelength long at

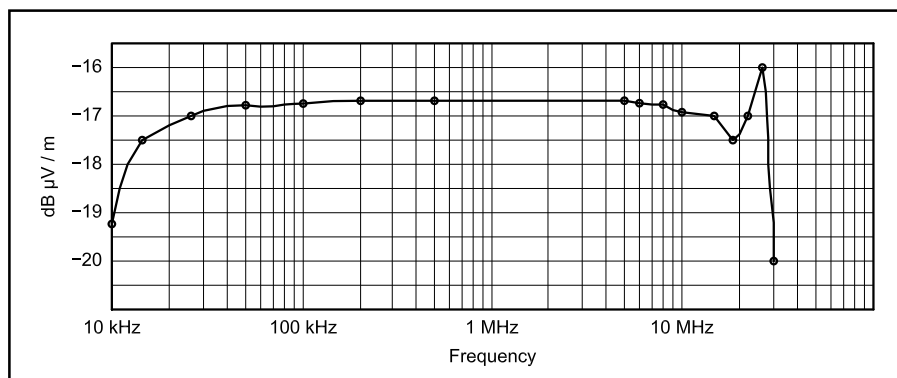


Figure 1—Active antenna response curve.

¹Notes appear on [page 37](#).

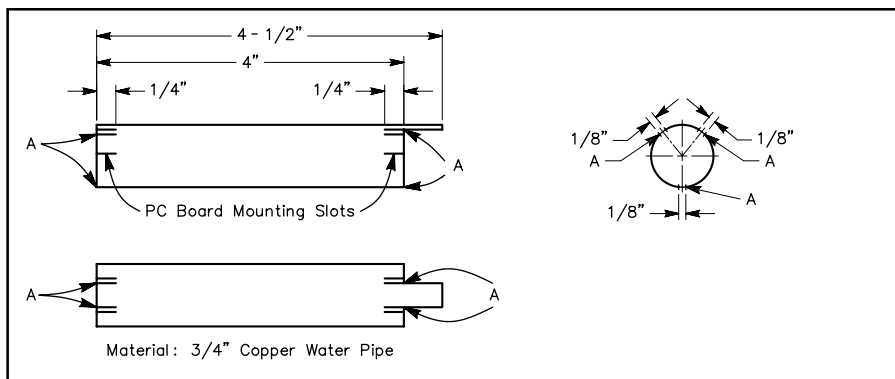


Figure 2—The heat sink is made from a 4½-inch piece of ¾-inch copper pipe cut and shaped as shown. Cut pairs of ¼-inch deep slots at the “A” points indicated. These form tabs that center the pipe in the PVC tube (see text and [Figure 5](#)).

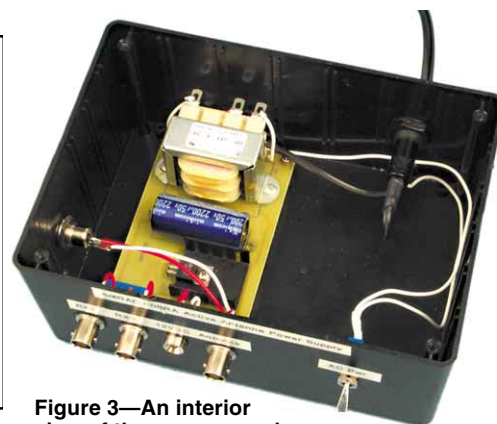


Figure 3—An interior view of the power supply enclosure and circuit board.



Figure 4—The amplifier, heat sink and PVC tube housing.

the desired frequency—connected to an active impedance-conversion circuit.

An electrically short whip has a high output impedance. For example, a 1-meter whip at 10 kHz has an input impedance of almost 2 MΩ. If such a whip were connected directly to a 50-Ω load, signals reaching the antenna would be attenuated almost 114 dB by the time they reached the receiver. The active impedance-conversion portion of this antenna is a high-input-impedance FET follower feeding a 50-Ω load, eliminating much of the signal attenuation. In this design, the attenuation is only about 16 dB. Reducing the non-linearity and the resulting IMD products was the major design challenge.

Although the Burhans antennas have IMD performance that exceeds that of many active antennas, urban hams need even better performance. After trying a number of changes to Burhans’ designs, we found that performance could be improved by increasing the level at which

clipping began and by using a more linear transistor. The problem with increasing the clipping level is that the transistor operating voltage and the bias current almost certainly increase, resulting in increased power dissipation by the transistor.

Simultaneously, we received some key design details from Dr Dallas Lankford, who was working on an HF antenna.⁸ He identified the Crystalonics CP-640/CP-650 series of junction FETs as outstandingly linear for active antenna applications. He was kind enough to share his design ideas and provide help with our IMD measurements. AMRAD kudos go to Dallas for his assistance.

The increased transistor heat dissipation is handled by a homemade heat sink constructed from ¾-inch copper pipe. Readily available PVC pipe fittings make a protective enclosure for the antenna.

A PC-board prototype was built using a resist pen printed circuit board and, after a few trials and changes, the antenna

performed well up to 30 MHz. Three additional antennas were built and used in AMRAD’s annual LF expedition to North Carolina’s Outer Banks—an environment that has low LF noise and superb LF propagation from Europe (as observed by monitoring European LF broadcast stations). The singular problem is a Coast Guard Loran-C transmitter at Carolina Beach, North Carolina. It operates on 100 kHz, transmitting short, 600-kW pulses.

During the Outer Banks expedition, the new antenna performed well. It was so good that the receiver, a modified Ten-Tec RX-320, became the limiting element.⁹ A 136-kHz filter placed between the antenna and the receiver solved the receiver IMD problem and brought receiver sensitivity down to the local noise floor.

Power Supply

The power supply (see Figure 3) is designed to minimize coupling between the power line, the antenna and station ground. The power transformer chosen is the result of carefully testing and sorting commercially available transformers. Similarly, the signals from the antenna are coupled to receiver ports **RX1** and **RX2** through a wideband isolation transformer, T2. This prevents noise on the receiver ground from coupling into the antenna ground. Isolation transformers such as this have been invaluable in reducing noise coupling in LF receiving systems.

The power supply has a provision (J4) for using an external 24-V dc source (ie, a battery) for portable operation. 1- or 2-Ah gel-cells provide power for several hours given the 53-mA load.

The antenna is designed to work into a 50-Ω load. Ideally, a 50-Ω receiver is attached to **RX1** and a high-impedance device, such as an oscilloscope or counter, is connected to **RX2**. Although the output impedance of **RX1** and **RX2** is about 14 Ω, a load less than 50 Ω degrades the IMD performance. Running multiple receivers on a single antenna has

turned out to be very handy at times.

Performance

This antenna achieves very good intermodulation and overload performance at some sacrifice in output level. The AMRAD amplifier is based on Burhans' noiseless feedback design. The frequency response curve for the antenna with a 1-meter whip is shown in [Figure 1](#). The input capacitance of the active amplifier is about 29 pF.

AMRAD member Steve Ratzlaff, AA7U, helped measure the second- and third-order intercept points. Overload and intermodulation performance are measured much as they would be for an RF amplifier or receiver.¹⁰ For second- and third-order intercept point measurements, a hybrid combiner is used.¹¹ We used a lower-frequency transformer for the hybrid that consisted of 25 bifilar turns of #30 wire on an Amidon FT-87-J ferrite toroid core.

Test signals were fed through a 12-pF capacitor to simulate the source impedance of a 1-meter whip. Referenced to the antenna output, the following values were measured: 1-dB compression point, +25 dBm; second-order intercept point, +53 dBm; third-order intercept point, +37 dBm.

The performance of the AMRAD antenna considerably exceeds that of every readily available active antenna we tested. You can expect similar performance, save for the last 5 dB or so of second-order IMD performance, which may have to be squeezed out using a test setup to fine-tune the bias current.

The second-order intercept point relates to the antenna's distortion product (f1-f2). Second-order intercept values often take a back seat to the more commonly measured third-order values. They become important in LF listening, however, because second-order distortion products can create spurious signals in the LF band in the presence of two local AM broadcast stations; the higher the number, the lower the distortion level. This number in no way implies that the antenna can withstand a signal-input level of +53 dBm, much less perform usefully under such conditions.

Construction

You can build the antenna using readily available hand tools. The PC boards are available from FAR Circuits.¹² The only required adjustments are setting the power supply voltage to 24 V and setting the amplifier transistor bias for a source current of 53 mA.

Q1 is special and available only from Crystalonics, which specializes in high-performance RF devices. Although the



The active antenna is housed in a Schedule-40 PVC tube with connections at opposite ends for the whip antenna element and the coaxial cable to the power supply and receivers.

company usually doesn't sell single devices, it has kindly agreed to sell them to readers of this article.

PVC Case

Prepare the pieces of Schedule 40 PVC pipe as follows:

Cut an 8-inch-long piece of 1-inch Schedule 40 PVC pipe (the amplifier case). Drill a 1/4-inch hole in the center of a 1-inch PVC pipe cap. This will become the top of the amplifier case. Similarly, drill a 3/8-inch hole in the end of a 1-inch Schedule 40 pipe cap. Drill a 9/64-inch hole in the end of the cap near the edge, 0.50-inch from the center. Countersink this hole for a #6 brass flat-head grounding screw. Cut two 1-inch-long pieces of 1/2-inch PVC pipe to act as spacers at the top and bottom of the printed-circuit board.

Place the BNC connector in the pipe cap via a 3/8-inch hole with the connector facing outward. Solder a short piece of #24 bus wire (approx) to the head of a #6 × 1-inch brass screw. Install the screw with the threads facing out. Solder the wire to the ground tab of the BNC connector. Solder a 1 1/2-inch piece of wire to a 1/4-20 × 1 1/2-inch brass bolt. Install it in the other PVC cap and seal it with Permatex *Silicone Windshield and Glass Seal*, available at auto parts stores, to seal the bolt, nut and washers to the PVC cap. This sealer is thinner than regular silicone sealer and flows into cracks and crevices for a better seal.

Note that the RadioShack BNC chassis connectors specified for this project are different than common chassis connectors. They have a small solder lug on the edge of the ground side that is used to connect the ground side of each signal line from the printed-circuit board. The ground tab cannot be bent out to make soldering easier. *It will break off.*

Tip: When mounting a BNC connector in plastic, apply a few drops of super glue (cyanoacrylate cement) to the edge of the connector next to the plastic. Rotate the connector a turn or so to distribute the cement along the joint where the connector meets the plastic. Tighten the nut and the connector will bond into place. While in service, the connector will not rotate when the bayonet connector ring is engaged or disengaged.

Place the two end caps on the 8-inch piece of pipe and make two small marks where the pipe caps meet the edge of the pipe when fully seated. Use these marks during final assembly to make sure that the caps are well seated on the pipe.

Heat Sink

Refer to [Figure 2](#) while building the heat sink. Cut a 4 1/2-inch piece of 3/4-inch copper pipe. On one end cut two slots 1/2-inch-long spaced 3/8-inch apart. Place the assembly in a vise and cut off 1/2-inch of the end of the pipe; leaving a tab. Do this by cutting around the pipe so that the tab remains between those slots. The tab that remains should be 1/2-inch long and 3/8-inch wide. This tab will contact the transistor case to help dissipate heat.

Cut two slots 1/4-inch deep and 180° apart on the tab end, placing the tab halfway between the slots. Cut two more slots on the opposite end of the pipe at the same position as the slots on the tab end. The metal next to these slots will be bent inward slightly to hold the PC board in place.

To keep the copper heat sink from rattling against the PVC pipe enclosure, cut six 1/4-inch-deep slots on each end to form six small tabs. Bend these out slightly, as shown in [Figure 5](#).

Active Antenna PC Board

The antenna's schematic is shown in [Figure 6](#). Make the wideband transformer

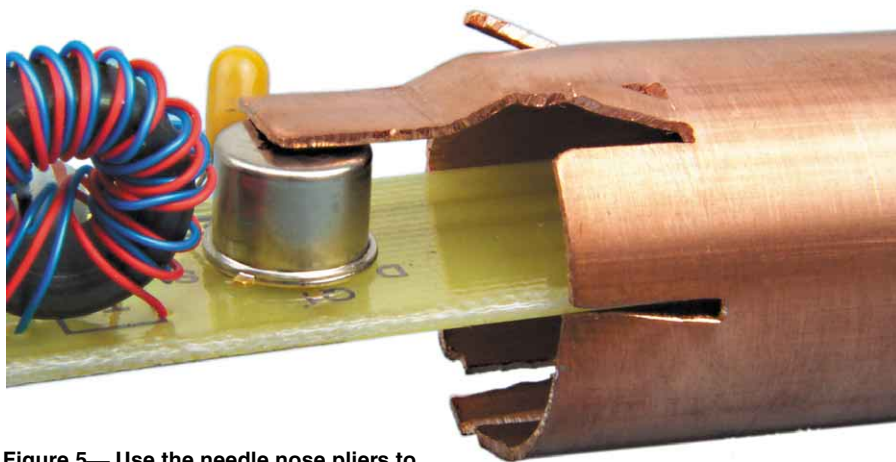


Figure 5—Use the needle nose pliers to bend the heat sink tab so it lays flat on the transistor case. Carefully bend the tab to maximize contact.

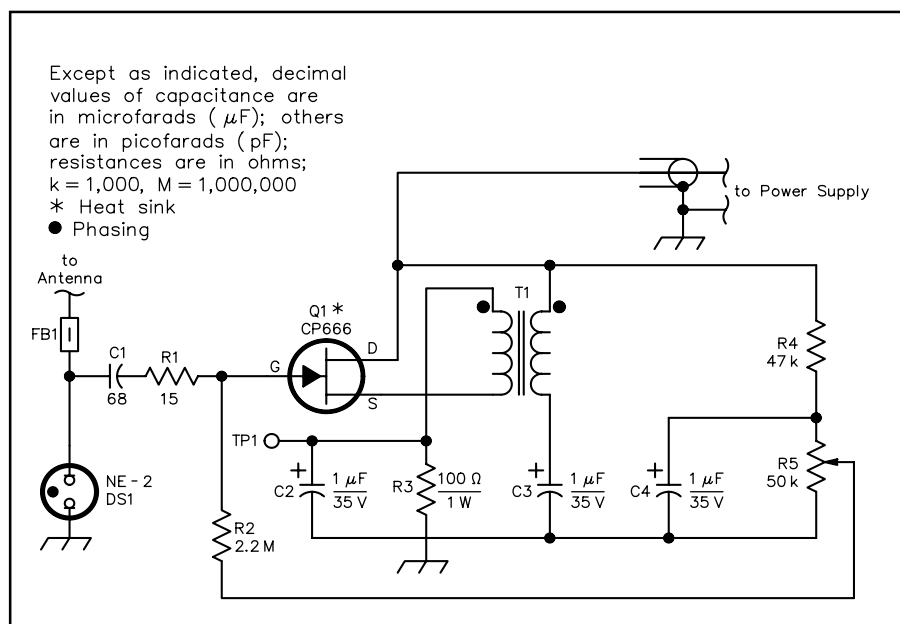


Figure 6—Active antenna schematic. Unless otherwise specified, resistors are $\frac{1}{4}$ -W, 5%-tolerance carbon-composition or metal-film units. Part numbers in parentheses are from RadioShack. Equivalent parts can be substituted.

C1—68-pF ceramic capacitor, 2 kV.
C2-C4—1- μ F, 35-V tantalum (272-1434).
DS1—NE-2 neon lamp (272-1102).
FB1—Ferrite bead, Amidon FB43-287.
J1—BNC jack (278-105).
Q1—CP-666 JFET (Crystallonics Inc, 17 A St, Burlington, MA 01803; tel 781-270-5522, fax 781-270-3130; www.crystallonics.com. When ordering, refer to this QST article.

International orders accepted. Price: \$14.75 plus shipping.)
R1—15 Ω ; see text.
R2—2.2 M Ω .
R3—100 Ω , 1 W (271-152).
R4—47 k Ω , (271-1342).
R5—50 k Ω potentiometer.
T1—17 bifilar turns #30 AWG wire wrapping wire (278-501) wound on an Amidon FT50-75 or FT50-J core.

by twisting two 18-inch-long pieces of #30 wire wrapping wire together. The wires should be different colors so they can be identified after winding. Wind 17 turns of the bifilar wire on the Amidon FT-50-J or FT-50-75 ferrite core. Note that the first time the wire passes through the center of the core counts as turn number one. Each additional time the wire passes through the core is considered an addi-

tional turn. The transformer design was optimized to avoid core saturation at maximum signal levels while having good VLF response. Adding turns will degrade the intermodulation performance. Sensitivity at 10 kHz is quite adequate.

Insert and solder the parts. Insert the wideband transformer wires so that the lead from the start of each winding is inserted in the PCB holes identified with

the dots. Insert the lead from the finish of each winding into the PCB transformer holes without the dots, keeping the primary and secondary windings connected as in Figure 6. Use different wire colors to distinguish the primary and secondary wires. When the PCB is completed, wideband transformer T1 can be secured to the board using a dab of silicone sealer.

Positioning the assembly on a hard, flat surface, carefully flatten the heat sink tab with a hammer. Slide the heat sink over the PC board and, using needle nose pliers, twist the pipe in at the slots under the heat sink so the board rests on the “shelf.” See Figure 4.

Use the needle nose pliers to bend the tab so it lies flat on the transistor case. Carefully bend the tab to maximize contact. See Figure 5. You may need to remove, adjust and replace the parts several times to get the tab positioned correctly. *This part of the assembly is very important!* Be patient and be sure to get this right so the transistor doesn’t burn up. The slots on the opposite end are bent inward slightly to form another “shelf.” This shelf will press in the opposite direction and cause the PC board to bend slightly so that the PC board acts as a spring and holds the transistor against the heat sink tab.

Slide the 8-inch piece of PVC pipe over the PC board. Adjust the three small tabs on each end of the heat sink (shown as “A” on Figure 2) to make the heat sink snug inside the pipe. Remove the PVC pipe and set it aside.

Solder a 4-inch-long piece of wire to the antenna pad of the PC board. Wind the wire through the holes near the pad to relieve the strain on the solder pad. Use a small dab of silicone to secure the wire in the holes.

Solder two 4-inch pieces of wire (different colors) to the signal connector pads on the other end of the PC board. Wind them through the nearby holes to act as a strain relief for the solder pads. Use a small dab of silicone to secure the wires in the holes.

Slide a 1-inch-long piece of $\frac{1}{2}$ -inch PVC pipe over the signal leads. Check the fit over the ground screw and file a clearance area on the edge of the spacer, if needed. Now trim and connect the signal leads to the BNC connector in the PVC pipe cap. Use small dabs of silicone sealer on the BNC connections to seal them and to provide strain relief. *Remember, the tab won’t bend without breaking!*

Slide the 8-inch PVC pipe over the PC board and down into the BNC connector pipe cap. Place the other one-inch-long piece of $\frac{1}{2}$ -inch PVC pipe over the antenna end of the PC board. Make sure that everything fits and that the antenna end



The active antenna power supply enclosure with BNC jacks for the coaxial cables to the active antenna and receivers.

Use small dabs of silicone sealer at the four points where the heat sink tabs contact the PC board to secure the heat.

Install the PVC pipe onto the amplifier. Place the 1-inch-long piece of $\frac{1}{2}$ -inch PVC pipe over the wire from the printed circuit board. Slide a ferrite bead over the wire. Use a short piece of insulated sleeving to slide over the solder joint and solder to the wire from the top cap. Shape the wire into a springy coil so it will fit into the stand-off tube. The top cap can now be slid over the PVC pipe. Use the mark on the pipe to make sure that the cap is fully seated and not pinching the antenna wire. Use caution when rotating the pipe caps during assembly or disassembly so the wire leads remain untwisted.

The assembly is now ready for outdoor testing with an attached whip. Connect a BNC coaxial jumper between the active antenna and the antenna connector on the power supply. Caution: Connect only the active antenna to the power supply connector. Receivers and other devices can draw excessive current and burn out L1 or damage the connected equipment. If, when connected, the choke burns out, the LED on the power supply will not light up. You may want to wrap a piece of colored tape near the end of the coax going to the active antenna to identify it as the correct cable. Connect a receiver to the RX1 or RX2 connector.

You should hear AM broadcast and HF signals. LF signals and noise should be heard when the receiver is tuned to the LF range. When you're satisfied that everything is working properly you can take down the antenna and seal the assembly.

Final Assembly

Once the caps are properly seated the amplifier can be sealed using silicone. Permatex *Silicone Windshield and Glass Seal* is thinner and will fill joints better than the more familiar silicone caulking. Seal around the top bolt, the top and bottom cap and the ground screw. After the goop hardens overnight the antenna amplifier is ready to install. To regain ac-

cess to the printed circuit board, peel the silicone sealer from around the edge of the pipe caps and force them off the PVC pipe by hand.

Several different whips can be used on the active amplifier. Short automobile replacement whips made to attach over the stub of a broken auto antenna can be found in most auto parts stores. One-meter stainless steel whips are available from RadioShack (21-952A). The RadioShack whips have $\frac{1}{4}$ -20 studs, so a $\frac{1}{4}$ -20 threaded sleeve is needed to mate the whips to the bolt stud on the top of the active amplifier. We used a stainless steel $\frac{1}{4}$ -20 T-nut for this purpose.

Up-to-date details on construction, assembly and testing can be found at www.amrad.org/lf/active.

Siting and Installation

This small antenna can be mounted almost anywhere, but an electrically quiet site will produce the best results. Rooftop vent pipes work well because the PVC vent pipes and the PVC antenna housings camouflage one another. Thin whips also disappear at a distance.

Use the ground screw next to the antenna BNC connector to establish a quiet ground reference for the antenna. This ground usually works best if it's *not connected to any other ground*. Testing various ground rod locations while monitoring LF noise on the receiver can help you pinpoint the best location for minimizing received ac power-line noise. Because of the low capacitance of the antenna and the coupler, a 12-inch ground rod may be satisfactory. A sheet of chicken-wire screening can be laid beneath the antenna and connected to the antenna ground to stabilize the fields around the antenna to further reduce noise coupling. Chicken-wire screening in rooftop installations is generally hard to see from the ground.

One source of intermodulation of which the US Navy is especially aware is the "rusty bolt" effect. When a corroded joint exists between two pieces of metal, the joint can act as a nonlinear

junction. In a strong RF field, the corroded junction creates intermodulation between the strong signals. On a ship (with its many transmitters) or in an area with several strong AM broadcast stations, the intermodulation is reradiated and receiving antennas, including this active antenna, can pick it up. This problem appears as LF carriers that have two sources of audio modulation. When these carriers are tuned in with an AM receiver, it sounds as though two stations are talking simultaneously. If this problem occurs, move the antenna or find and clean the offending joint.

A block of wood with wedges cut in it can be used between the antenna and a mast. Use a stainless steel hose clamp to secure the assembly. Avoid placing metal hose clamps or other metal objects near the upper half of the antenna as nearby metallic objects can add to the input capacitance and slightly degrade the antenna performance.

Keep the coax run to the shack insulated from any grounds as it wends its way to the power supply. With such low capacitance between the power line and the receiver grounds, it's important to minimize parasitic noise coupling in the antenna ground circuit by keeping the line away from other grounds and power lines.

Best LF performance is obtained if the antenna whip is higher than nearby conducting objects. Imagine pulling a giant plastic sheet over your house and yard. The whip should be above this imaginary sheet. A more accurate (and much more complex) way to think of it is to imagine a large metal sheet several hundred feet above your house and yard (play along). Now imagine that the sheet is charged with a high dc voltage. If you were to examine the electrostatic field around and above your house and yard, you would discover that those points below the plastic sheet are at a 0-V field potential.

LF signals have very long wavelengths: at 136 kHz, 1 wavelength is 7181 feet. At these wavelengths, the average suburban yard is less than $\frac{1}{10}$ wavelength across, so an electrostatic field may be used to approximate LF waves. Thus, at LF, those areas with a zero electrostatic field will also have a zero, or near-zero LF field strength. The freely downloadable student version of the QuickField Finite Element Analysis program (www.quickfield.com) can be used to plot the electrostatic field around a simple house and yard model.¹³ Or, as mentioned above, simply visualize the plastic sheet and make sure the antenna isn't mounted "underneath" the imaginary boundary...

Measuring Field Strength

This active antenna has reasonably re-

producible sensitivity when the PC boards and listed parts are used. This makes it possible for you to measure signal strength in volts-per-meter, which means that the overall efficiency of an LF antenna can be measured rather than estimated.

Using a receiver S-meter and a signal generator, the signal voltage from the antenna can be measured by substituting the signal generator for the antenna and adjusting the signal generator to get an identical S-meter reading. A selective voltmeter that can directly indicate the voltage at a received frequency is even better. Once the antenna output voltage is known, the field strength can be calculated by using the antenna factor, which is added to the antenna-voltage reading, to give the field strength in volts-per-meter. When using the antenna for measuring field strength, avoid using any metal clamps or other metal around the upper half of the antenna.

If you are using dBm to express voltage and dB μ V/m (dB μ V/m = dB above 1 microvolt per meter) to express field strength, the antenna factor is -16.5 dB μ V/m. If you want volts-per-meter, multiply the measured voltage by 6.683 to convert to volts-per-meter. This antenna factor is accurate (for this antenna) between 20 kHz and 26 MHz (see Figure 1). Keep in mind that this isn't an individually hand-calibrated EMC antenna, so use the results with care. Above 10 MHz, measurements become questionable with any E-field antenna and become more subject to minor construction variations.

Variations on a Theme

A standard 108-inch CB whip with a $3/8$ -24 stud can be mounted to the active amplifier using a RadioShack " $3/8$ -24 to Lug Mount adapter" (21-950). This large whip needs a firmer attachment at the top cap. Use $1/4$ -inch-diameter brass washers on each side of the pipe cap on the $1/4$ -20 bolt. The bolt length may need to be reduced to match the thread length inside the $3/8$ -20 adapter. Use plumbers PVC cleaner and PVC cement to firmly attach the cap to the pipe. If you later need to access the PC board you'll have to saw off the top and make another PVC housing.

If low-band VHF or TV Channels 2 or 3 are particularly strong in your area, you may need to add two or three ferrite beads on the wire between the amplifier and the whip. These added beads roll off the response starting at about 10 MHz rather than 30 MHz, providing greater attenuation at the low-VHF range. In place of using R1, another choke can be added to further reduce the higher-fre-



A sheet of chicken-wire screening can be laid beneath the antenna and connected to the antenna ground to stabilize the fields around the antenna to further reduce noise coupling. Chicken-wire screening in rooftop installations is generally hard to see from the ground.

quency response.

If connector confusion could lead to connect 24 V where it shouldn't be, substitute an F, TNC or Mini-UHF connector for the antenna BNC connector.

The length of the PVC pipe can be made longer and the whip contained inside along with the PC board. It then can be mounted on a windowsill and disguised as a flagpole to hide its true purpose.

If you require less capacitive coupling to the power line, you may be interested in knowing that we tested a Tamura 3FL30-200 transformer and found a capacitance of only 14.7 pF between the two 120-V primary windings. If this model is used as an outboard isolation transformer, the combined capacitance between the power line and the dc supply is reduced to only 9.25 pF. This applies only if you are using the 120-V connection. We haven't yet seen the need for such a low capacitance, but it's comforting to know there is a solution if one is needed.

Acknowledgments

Many people helped with this project, and the AMRAD lunch crowd attendees who eat tacos and talk Amateur Radio at 12:30 each Saturday at Tippy's Taco House in Merrifield, Virginia, certainly contributed their share. Come by and see us and talk about LF while chowing down on a basket of tacos. Thanks go to Ralph Burhans, who set out a clear discussion of active antennas in his writing; Chuck

Rippel, WA4HHG, who provided key comments and encouragement; Steve Ratzlaff, AA7U, who provided a number of useful suggestions on the design and conducted the antenna's intermodulation testing. And finally, Dallas Lankford must be recognized for providing key help on the design, especially the CP-666 transistor.

It is with sadness we note that Ralph Burhans passed away in May 2001. He had indicated his interest in our active antenna project until his death.

Notes

¹Dick Goodman, WA3USG, "The Monster Loop," *QST*, Sep 2000, pp 38-40.

²Bill Farmer, W3CSW, "Attic Loop Antenna," *AMRAD Newsletter*, Nov-Dec 1999, pp 4-5; available at the AMRAD Web site LF page, www.amrad.org/projects/lf.

³Ken Cornell, W2IMB, "Varactor Tuned Remote Active Antenna," *The Low and Medium Frequency Radio Scrap Book*, 8th Edition, Ken Cornell, Point Pleasant Beach, NJ, 1992.

⁴Andr Kesteloot, N4ICK, "A Remotely-Tuned Active Antenna for LF," *AMRAD Newsletter*, Nov-Dec 1998, p 10.

⁵Ralph Burhans, "All About VLF Active Antennas," *Radio-Electronics*, March-June 1983, pp 63-68.

⁶Ralph Burhans, "Active Antenna Preamplifiers," *ham radio*, May 1986, pp 47-54.

⁷Frank Gentges, K0BRA, "Annapolis Report," *AMRAD Newsletter*, May-Jun 1999, pp 8-10.

⁸Private e-mail with Dr Dallas Lankford, Professor, College of Engineering and Science, Louisiana Tech University.

⁹Frank Gentges, K0BRA, "Modifying the RX-320 Receiver for LF/VLF Operation," *AMRAD Web site LF page*, www.amrad.org/projects/lf.

¹⁰"Receiver Performance Tests," *The 2001 ARRL Handbook for Radio Amateurs*, p 26.45.

¹¹"Hybrid Combiners for Signal Generators," *The 2001 ARRL Handbook for Radio Amateurs*, p 26.40.

¹²FAR Circuits, 18N640 Field Ct, Dundee, IL 60118-9269; tel 847-836-9148. Price: \$8.50 per set plus \$1.50 shipping for up to four boards.

¹³Frank Gentges, K0BRA, "How Low is LF?" *AMRAD Technical Symposium 2000*, pp 69-79.

Frank Gentges, K0BRA, was first licensed in 1956 as K0BRA. He upgraded to Extra Class in 1964 and was later licensed as W3FGL and AK4R, but chose to reclaim his old call sign when the FCC made that possible. He became an associate member of ARRL in 1953 and became a full member in 1956. He graduated as an Electrical Engineer from Kansas State University in 1965. After school he worked for Rixon Electronics, followed by the US Navy, where he retired in 1987. Frank is now president of Metavox, which develops new tactile technology for profoundly deaf infants. You can contact Frank at 9251 Wood Glade Dr, Great Falls, VA 22066; fgentges@mindspring.com.

QST